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**LOW PROFILE MAGNETIC ELEMENT****Cross Reference to Related Applications**

Priority is claimed from U.S. provisional patent application Serial No. 60/372,279 entitled "Low Profile Magnetic Element" filed April 12, 2002 in the name  
5 Ionel D. Jitaru and Marco Davila. That application is incorporated herein by reference.

**Field of the Invention**

This invention relates to mechanical construction and its electrical results for planar inductors and planar transformers used in power conversion.

**Background of the Invention**

10 The industry demand for increasing power density and lowering the height of power converters imposed the use of planar inductors and planar transformers. The continuous trend for lower voltages and higher current has set new challenges for power magnetic components such as transformers. In order to simplify and control the manufacturing process for power magnetic components, the windings are embedded or  
15 buried within multilayer PCB structures. In such applications the copper thickness is limited. This limitation will exclude applications wherein large currents are processed, which today is the growing trend. One solution to overcome this problem is to split the current and process each section of it before it is provided to the output. Because the power dissipated due to the DC impedance is proportional with the square of the  
20 current, splitting the current, for example in two sections will reduce by a factor of four the power dissipation due to the DC impedance. Another limitation comes from the semiconductor devices. The trend towards miniaturization has forced the design to use surface mounted, smaller packages for semiconductor devices. These devices will accommodate only a limited die size, i.e., a semiconductor layer or layers of limited  
25 size. As a result, such devices provide only a limited current capability.

In Fig. 2 appears a prior art approach of splitting the output current wherein several transformers are employed. The primaries 16, 20 and 24 of the transformers 10, 12 and 14 are in series and the currents in secondaries 18, 22 and 26 are processed in

parallel. The secondary windings can be placed in parallel directly or paralleled after the rectifiers (not shown). This concept, also described in US patents of Jitaru Nos. 5,990,776 and 6,046,918, both incorporated herein by reference, offers several advantages. First it splits the output current, which is further processed (rectified) on parallel paths, before it unites at the output of the converter. By placing several transformers in series the voltage across each primary winding is decreased, and as a result the number of turns in the primary winding can be reduced. A reduced number of turns will decrease the leakage inductance, which is proportional with the square of the number of turns. The use of smaller transformer, and as a result, a smaller magnetic core, will allow a better cooling due to an increased core surface area to volume ratio, will decrease the eddy current losses in the magnetic core due to a thinner core, and will prevent the electromagnetic resonant losses associated with very large magnetic cores.

One major drawback of this concept is the fact that the magnetizing inductance is lower, leading to larger magnetizing current and as a result lower efficiency. This is due to the fact that the magnetizing inductance is proportional with the square of the number of turns, and the total magnetizing inductance for the magnetic structure from Fig. 2 is the summation of all the magnetizing inductances. If there are used "n" independent transformers each of them with a number of turns in primary "N", the magnetizing inductance of the structure is  $L_m = nKN^2$ .

There remains therefore a need for an improved magnetic component with a better core and winding relationship. In particular, there remains a need for a transformer structure that splits the secondary current for parallel processing, uses a small core wound with series-connected primary windings, and produces an increased magnetizing flux for higher efficiency.

## Summary of the Invention

The magnetic component structure of this invention provides an improved magnetic core and winding arrangement. For transformer construction, it is highly suitable for higher current applications. The invention will allow a reduction in the core volume while the current in the secondary is split to minimize the conduction losses. As

a consequence the invention leads to lower core loss, and lower conduction losses in a transformer structure.

In the structure depicted in Fig. 3, according to this invention, a number "n" of transformer windings are linked by the same flux and therefore  $L_m = K(nN)^2$ . The result is a much larger magnetizing inductance, lower magnetizing current and, consequently, lower losses.

In accordance with the invention, a magnetic circuit element includes a circuit board with at least two flux-conducting magnetic core arms or segments penetrating the board and at least two flux-conducting magnetic elements extending between the core arms on opposite sides of the board. At least one buried winding carried on an interior intermediate layer of a multilayer circuit board encircles or partially encircles one of the core arms or segments. The core arms and elements cooperate to form a flux path that is closed and unbranched. By "closed" is meant a flux path that returns upon itself as does the combination of C and I core sections; the term is not meant to exclude air gaps although the specific preferred exemplary embodiments described in detail below are without air gaps.

In the preferred embodiment of a transformer in accordance with this invention, at least two series-connected primary windings are imprinted or deposited on the board in encircling or partially encircling relation to at least one of the arms and at least two parallel-connected secondary windings are printed or deposited on the board in encircling or partially encircling relation to at least one of the arms. The board preferably is a multilayer circuit board and one or more of the windings are printed or deposited on a surface of a layer intermediate the outer surfaces of the board as buried windings. Preferably all of the windings are thus buried. In a preferred exemplary embodiment, the structure includes circuit components including one or more active or power components occupying locations on at least one of the outer surfaces of the circuit board directly above or below at least one of the buried windings, thus providing high power density.

The core sections that make up the magnetic flux path in accordance with the embodiments of the present invention are referred to variously as core elements,

segments or arms. The core pieces that extend generally parallel to the faces of the board have been referred to as core "elements." These may be planar as that term has become known in the art. I.e. these parts of the magnetic core can be "planar" in being low in profile and extending along the surface of a circuit board with a low generally planar upper surface so as not to greatly increase the circuit thickness. The terms "segments" and "arms" have been used to refer to the core sections located in holes in the circuit board, penetrating the board from one outer face to the other. The core "elements" and "segments" or "arms" are not necessarily distinct or separable pieces of the core. For example, when the core is formed in whole or in part of "C cores" or "C core sections," these "elements" are the integral spanning central part of the "C" that joins together the two parallel arms of the C, the bight as it were. In that case the two ends of the C are the segments or arms that penetrate the board.

Preferably, in one transformer formed in accordance with the invention, every primary winding that is connected in series has the same number of turns as every other primary winding. Likewise, every parallel-connected secondary winding has the same number of turns as every other secondary winding. Preferably, each primary winding is closely coupled to a secondary winding.

The magnetic core of this invention has a good surface to volume ratio. The absence of intermediate branching flux paths permits greater space for the windings inward of the closed magnetic circuit that the core forms. Each core arm penetrating the board and each core element bridging a pair of core arms can be fashioned from a magnetic C core section or a magnetic I core section. In one particular exemplary embodiment, the core elements bridging the penetrating core arms comprise a pair of magnetic plates overlying the two exterior surfaces of the circuit board. In this embodiment, each plate may be in flux conducting relation to all of the core arms penetrating the circuit board.

The invention includes, in a preferred exemplary embodiment, the method of power conversion for providing high amperage, low voltage power including the formation of a printed circuit board, forming holes through the board, locating magnetic core arms in those holes, locating magnetic core elements in flux-conducting relation between the arms on opposite faces of the board to form a transformer core, and winding on the core arms a plurality of series-connected windings and a plurality of

parallel-connected windings on the core arms to form, respectively, a transformer primary and a transformer secondary. Preferably, winding the plurality of series-connected windings and parallel-connected windings is by printing or depositing the windings on surfaces of the board in encircling or partially encircling relation to a core arm. Preferably, too, the printing or depositing of the windings, at least in one or more occurrences, is again on a surface of a layer that is to be located intermediate the outer surfaces of the board, whereby these windings become buried windings in a multilayer circuit board.

The invention preferably includes a multilayer printed circuit board made by the foregoing process and having the characteristics described above. Such a printed circuit can accomplish high current high power density, good heat dissipation, and high magnetizing flux linking all windings for high efficiency.

The above and further objects and advantages of the invention will be better understood from the following detailed description of at least one preferred embodiment of the invention, taken in consideration with the accompanying drawings.

### Brief Description of the Drawings

Fig. 1A is a diagrammatic illustration of the prior art wherein two magnetic cores are utilized;

Fig. 1B is a diagrammatic illustration of an improvement of the prior art wherein only one magnetic core is employed;

Fig. 1C is a diagrammatic illustration of an embodiment of this invention;

Fig. 2 is a schematic illustration of the prior art transformer configuration for splitting the output current;

Fig. 3 is a schematic illustration of one embodiment of a transformer configuration according to the invention for splitting the output current;

Fig. 4 is a diagrammatic illustration of another embodiment of this invention for splitting the output current in four sections;

Fig. 5 is a diagrammatic illustration of another embodiment of this invention for further splitting the output current in "n" sections;

Fig. 6 is an exploded diagrammatic view that illustrates an embodiment of the invention and shows a mechanical construction of one embodiment of the present invention including a multilayer printed circuit board;

Fig. 7 is another exploded diagrammatic view and shows the mechanical construction of a further embodiment of the present invention;

Fig. 8 is a diagrammatic, partially exploded view illustrating the relationship of a multilayer board with a transformer formed in accordance with the invention; and

Fig. 9 is a schematic diagram, partially in block diagram form and illustrating the parallel treatment of secondary winding outputs.

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### Detailed Description

Turning to Fig. 3, a transformer structure 28 according to the invention is shown schematically. To split the output current, independent secondary windings are used, such as 32, 36... $n_s$ . Typically, for high current, these secondary windings have only one turn. Primary windings of the transformer 28 are also split in the same number of sections as the secondary. These sections 30, 34... $n_p$  are close coupled with their equivalent secondary 32, 36... $n_s$ . In this way a close coupling between primary and secondary is formed. The magnetic flux in a magnetic core 150 used by the structure 28 links all of the windings. For comparison, Fig. 2 is a schematic representing the prior art concept wherein independent transformer structures are used for splitting the output current. As mentioned before, in this prior art approach, the magnetizing current is lower and it leads to a larger magnetizing current and lower efficiency.

Fig. 1 demonstrates the transition from the prior art implementation to the structure of this invention. In Fig. 1A two transformers 42, 44 are formed by two E cores or by an E & I core configuration. Each transformer has a one turn winding 64, 66, which surrounds the center leg. In the transformer 42 flux through the outer legs 50, 52 of the magnetic core is shown. The flux 100, through the outer leg 50, and the flux 102, through the outer leg 52, unite into the center leg 54.

Fig. 1B illustrates an improvement of the original structure wherein the two transformers merge into only one, 46. There is a one turn winding 68, 70 surrounding or encircling each leg 55 and 56. The fluxes 108, 110 generated by the current flowing

through the winding 68 and 70 merge into the center leg 58 of the transformer. If the current flowing through the winding 68 is equal to the current flowing through the winding 70, the flux flowing through the center leg 58 is zero.

5 A first embodiment of this invention is, then, depicted in Fig. 1C. Since, for equal currents flowing through windings 68 and 70 of the Fig. 1B arrangement, the flux through the center leg is zero, the next step is to remove the center leg. In the case of the transformer 48 of Fig. 1C, then, the E core configuration of Figs. 1A and 1B is changed to a pair of C core (or C & I cores) to form the transformer core. The flux path formed, then, no longer branches. One advantage of this is an increase in the winding  
10 area 71, i.e. the area inside the core available for windings. Another advantage is a decrease in core loss due to a decrease of magnetic core volume. In Fig. 1C, a printed circuit board is indicated at 73. Vertical core arms 61 and 63 penetrate the board 73. The core 62, thus formed, is an unbranched or branchless core forming a closed flux path linking each winding 72 and 74 with the same flux 60.

15 In Fig. 4 an embodiment of the invention extends the concept depicted in Fig. 1C to a four winding structure, forming a magnetic structure 76. Windings 116, 114, 120 and 118 carry the same current. A flux 112 flows through the C cores 180, 186 and through the I cores 182, 184. Like the core structure of Fig. 1C, the core structure of Fig. 4 can be also constructed by using only C core members or only I core members,  
20 without departing from the spirit of the invention. The parallel arms 191, 192 and 193, 194 of the two C cores 180 and 186 are brought together end to end with the two coplanar I cores 182 and 184. This arrangement of the magnetic cores pieces resembles the assembled core pieces of Fig. 1C. Again, the same flux links all windings. The core is, once more, an unbranched, closed flux path. The core arms 191 - 194 penetrate a  
25 circuit board indicated as 195 on which the windings 116, 114, 120 and 118 may be printed or deposited to encircle or partially encircle the core legs.

Fig. 5 illustrates an embodiment of the invention that is a further extension of the concept described with respect to Fig. 1C. It illustrates how the concept of this invention can be applied to any number of windings that is a multiple of two. The  
30 current flowing through the depicted windings 124, 126, 128, 130, 132, 134, nn and mm is equal. This leads to an equal flux 138 flowing through each of the elements of the magnetic core. The magnetic structure 122, then, is a generalization of the concept

described with respect to Fig. 1C. The core 139 can be composed entirely of C or I members or combinations of the two. A circuit board is indicated at 140 and is of course penetrated by the core arms 150, 151, 152, 153, 154 -mmm, nnn, which are encircled or partially encircled by the windings 124, 126, 128, 130, 132, 134 -mm, nn.

5 The flux path is closed and unbranched. All windings are linked by the same flux.

In Fig. 6 an embodiment of the invention provides a mechanical configuration that offers practical application of the described concepts. It applies to a planar magnetic using a multilayer circuit board. The windings indicated by the dashed lines 171, 173, 175 and 177, are embedded into the multilayer circuit board 178. Multilayer  
10 printed circuit boards having electrically conductive buried windings at least partially encircling core portions that extend through the board are disclosed in the incorporated U.S. patent No. 5,990,776 of Jitaru. The windings here surround the holes 181, 183, 185 and 187. A series of cylindrical core arms 166, 169, 170, 172 made of magnetic material are placed into the holes 181, 183, 185 and 187. These serve as the arms of the  
15 magnetic core. Made also of magnetic material, a series of plate-shaped elements 162, 168, 174 and 176 is secured by conventional means to the tops and bottoms of the cylinders 166, 169, 170, 172 in the relationship shown. The configuration depicted in Fig. 6 is a practical implementation of the structure depicted in Fig. 4.

Fig. 7 illustrates a further embodiment of the invention in which the magnetic  
20 plates 162, 168, 174 and 176 of Fig. 6 are replaced by just two magnetic plate elements 190 and 192 affixed to the cylindrical core arms 166, 169, 170 and 172 at their tops and bottoms. The advantages of using standard building elements, magnetic plates and magnetic cylinders are numerous. First of all it offers an economical solution in addressing the magnetic design for different power levels. More elements are employed  
25 as a function of the output current requirements. The basic cell uses a core of just two plates and two cylinders. From this cell one can extend to as many winding outputs as needed.

In Fig. 8, layers 201, 202, 203 and 204 make up a multilayer circuit board 200. Magnetic core arms 210, 211 and 212 mask from view similar magnetic core arms 214,  
30 215 and 216. Openings 220, 221 and 222 form holes through the assembled board receiving the core arms 210, 211 and 212. The core arms 214, 215 and 216 are similarly received in holes through the board masked from view in Fig. 8.



About each of the core arms 210, 211, 212, 214, 215, and 216, is wound at least one winding 225 - 233. These are printed on the layers of the multilayer board and become buried windings. Magnetic core elements 240, 241, 242 and 243 extend parallel the upper and lower surfaces of the board. The magnetic core element 231 connects the ends of the core elements 210 and 211 in flux-conducting relation. The core element 234 connects the ends of the core arms 211 and 212 similarly. The core element 232 connects the core arms 212 and 216. A further, masked core element 235 lies behind the core element 234 in Fig. 8 and connects the ends of the core arms 216 and 215. Similarly, a masked core element 236 lies behind the core element 231 connecting the core arms 214 and 215. Finally, completing the magnetic circuit formed by the core members, the core element 233 bridges core arms 210 and 214. It will be appreciated that the core members, thus constructed, form a single, closed, unbranched flux path. Circuit components can be seen on the upper and lower faces 241 and 242 of the board 200. At least some of these elements lie directly over or under the buried windings 225 - 233. Of those, at least certain of the components such as the components 246 and 247 are active or power components, whereas others such as 248 and 249 are passive components. The lack of any branching core path and the availability of much of the upper and lower surfaces, even those above and below the windings, for location of circuit components contributes to excellent power density. The magnetic core, like those earlier described, can be formed entirely of C or I core pieces or of a combination of C and I pieces.

Fig. 9 illustrates schematically a preferred embodiment of the invention in which the transformer 300 is like the transformer of Fig. 3. Series-connected windings 301, 302 and 303 form the primary. Circuitry 310, 311 and 312 treats the output of the parallel-connected windings 314, 315 and 316 that form the secondary of the transformer. The circuitry 310, 311 and 312 is connected between the secondary outputs and current additive nodes 318 and 319 at which the secondary windings are connected in parallel. The circuitry 310, 311 and 312 may be only the typical rectifying diodes or may include additional current treating elements.

The foregoing descriptions of preferred embodiments are exemplary and not intended to limit the invention claimed. Obvious modifications that do not depart from

the spirit and scope of the invention as claimed will be apparent to those skilled in the art.